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PATENT

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Application No.:

10/666,168

Filing Date:

September 19, 2003

Applicant:

Phillip Martin Gibbs et al.

Group Art Unit:

3738

Examiner:

Bruce E. Snow

Title:

MODULAR PROSTHETIC HEAD HAVING A FLAT

PORTION TO BE IMPLANTED INTO A CONSTRAINED

LINER

Attorney Docket:

5490-000301

Director of the United States Patent and Trademark Office P.O. Box 1450 Alexandria, VA 22313-1450

DECLARATION UNDER 37 C.F.R. § 1.131

Sir:

We hereby declare under penalty of perjury as follows:

- 1. We are the inventors of the claimed subject matter of the subject patent application.
- 2. Exhibit A is a page from an engineering notebook that is dated and witnessed, with dates redacted, prior to January 3, 2002.
- 3. Before January 3, 2002, we conceived of and/or reduced to practice in the United States, a prosthesis system for implantation into an anatomy that includes a ball portion and a cup portion with an entrance. The ball portion has a portion with a dimension equal to or less than a dimension of the entrance to the cup portion. The ball

portion also has a portion with a dimension greater than a dimension of a concave area, as evidence by the following.

- The page in Exhibit A is entitled "Constrained Liner Idea" that illustrates, in the upper left-hand corner thereof, a liner with a ring that would interact with the liner and it is stated in Exhibit A a "liner that fits ordinary shells with ring that is installed at Biomet".
- 5. The page in Exhibit A also states that "the endo type head would have a small flat around the equator to allow it to go into the liner. The flat could be positioned in a way that the head would be unlikely to dislocate, but in a position that would allow a surgeon to position the leg to reduce the hip in surgery". This concept is further illustrated in the lower right-hand corner of the page as an exemplary head illustrated with a flat portion thereon.
- 6. Exhibit B is a R&D Work Request, with date information redacted that is evidence that parts were made by us or on our orders and delivered to us on or before January 3, 2002.
- 7. Exhibit B includes drawing prints showing configurations and dimensions of various head portions for a femoral head replacement that includes a reduced radius or "flat" portion.
- 8. Exhibit C is an "Investigational" router, with date information redacted, that illustrates a design of a liner that can include a ring positioned near an opening into an interior portion of the liner. Exhibit C includes a redacted start date before January 3, 2002 (on the first page) and a completion date of January 3, 2002 (shown as the date of "Inspect" on the last page of the "Investigation").

- 9. The liner illustrated in Exhibit C would allow, and was made for, insertion of a head portion, as illustrated in Exhibit B, to enter the interior portion of the liner when an axis of a the reduced radius area is aligned with an axis of the entrance.
- 10. Exhibit D is an Applied Technology Mechanical Test Request Form and accompanying drawings and test data, with proprietary data redacted. Exhibit D includes a Requested by W. J. Slone and a Date Submitted of January 3, 2002 and a Test Close-Out Information that illustrates that the requested tests were Conducted by K. Howard and Dated Completed was January 7, 2002.
- 11. Exhibit D includes a cover sheet that describes that two sets of liners, one with a Cobalt reinforcement ring and one with a titanium reinforcement ring were used with three different types of femoral heads in a lever-out test. The three heads were a 36mm full spherical, a 36mm full spherical with a 34.5 mm circumferential flat, and a 36mm full spherical with a 35.0 mm circumferential flat.
- 13. Exhibit D also illustrates that the various samples, Sample 4, Sample 5, Sample 12, Sample 13, Sample 6, Sample 7, Sample 14, and Sample 15, that clearly include the circumferential flats in a starting position and in a maximum load position relative to a liner that includes a constraining ring.
- 14. Exhibit A, with dates redacted illustrates a conception and/or reduction to practice of the subject matter of the claims in the subject application. Exhibits B and C provide evidence that the subject matter of the claims in the present application was reduced to practice and built on or before January 3, 2002. Finally, Exhibit D is evidence that parts embodying the subject matter of the claims of the present invention were tested on or before January 7, 2002

We hereby declare that all statements made herein of our own knowledge 15. are true and that all statements made on information and belief are believed to be true; and further that these statements are being made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application, and patent issuing thereon, or any patent to which this verified statement is directed.

Dated: 3-28-2006

Dated: 3-28-2006



Request Date:

Engineer:

Phil Gibbs

ext. 1690

Project Number:

Product Name: modular heads with flats

Make Per:











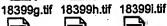
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Price Quoted

Time and Materials:

Instructions:

this research was originated to support constrnined liner development. by decreasing ROM slightly, we should be able to experience much greater pull-out and lever-out and still be able to assemble. question is increased wear concerns

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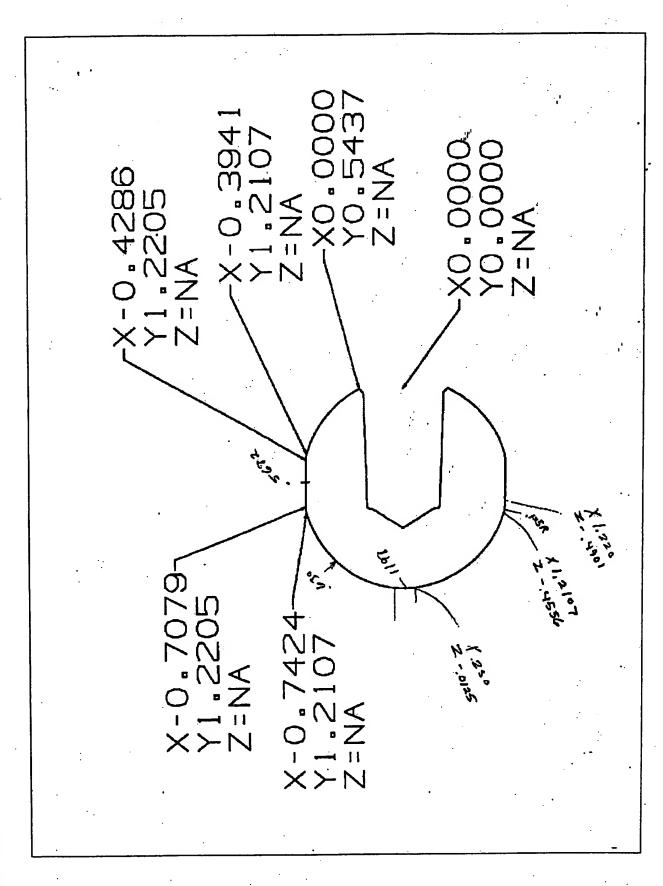
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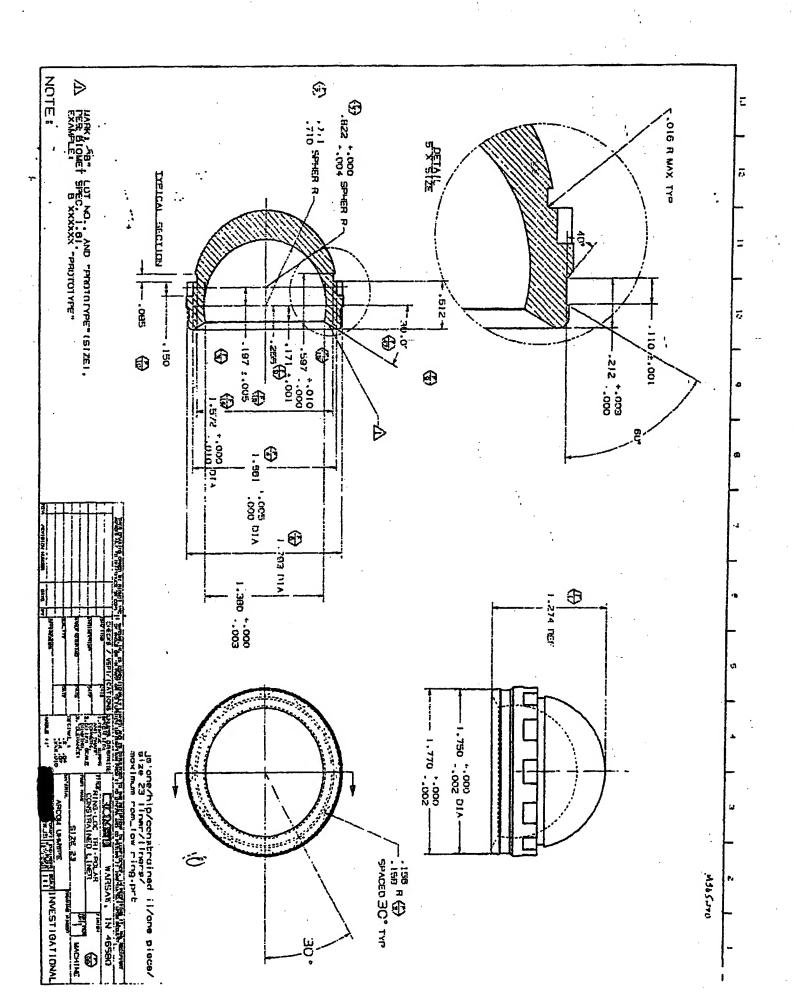
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Applied Technology Mechanical Test Request Form

тој	ect : Constrained Liner II	Project #:H	P000180			
l'itle	Lever-out with 3 different 36mm Co-Cr	Modular Heads				
Γes	Type: Fatigue X Static Other (specify)	Rotatin	g Beam	Wear		
Cor	ducted: X In-House Outside Lab (specify)	<u></u>				
Tes	t Components: (Part A is primary componer	nt for test)				_
-	Part Name	Part#	Lot#	Size		4
Ā	23 Constrained +5 Liner w/Cobalt Ring	Investigational	815390	23	6	4
B	23 Constrained +5 Liner w/Cobalt Ring	Investigational	815390	23	6	4
C	36mm Fully-spherical Modular Head	Investigational		36mn		4
D	36/34.5mm Fully-spherical Modular Head with 34.5mm circumfrencial flat	Investigational		36mm		
E	36/35.0mm Fully-spherical Modular Head with 35.0mm flat	Investigational		36mm	n 1	
	he test components are not finished production terial: ABCDE X Ti-6Al-4V	A BCDE	e wny. Stainless Steel	(type)		
	x Ti-6Al-4V .x x x x CoCr P85/15 P82/18	хх	UHMWPE LactoSorb Other (specify)			
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Specify differences between multiple specimens: The only difference between the two liners is the constraining ring. The liners themselves are from the same lot.

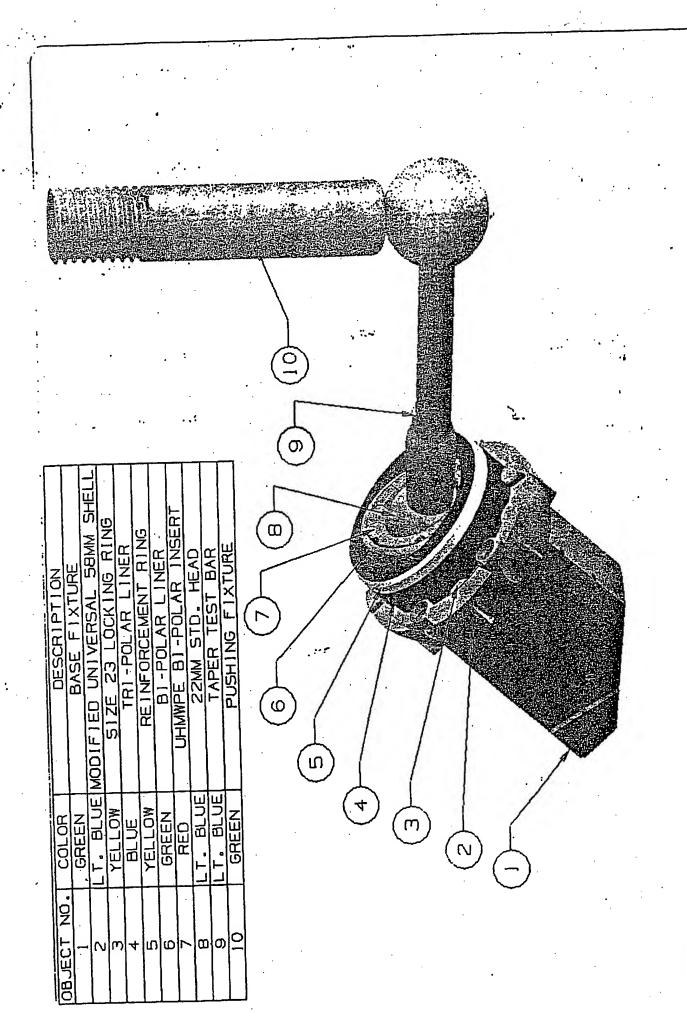
Objective(s) of Test: Determine the amount of torque required to lever-out three different 36.0 mm modular head designs from the liner, as well as determining how much if any a Cobalt Reinforcement ring will strengthen design from a Titanium Reinforcement Ring.

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Biomet Mechanical Test Lab Static Test Data Sheet

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Test #MIZTON Machine ID Raymons		
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LOT 815390 APPLY TO PATIENT RECORDS

Test Report MT-2439 Lever-Out with 3 different 36mm Co-Cr Modular Heads

Test Site:

Biomet Inc.

Airport Industrial Park Warsaw, IN 46580

Conducted By:

Kelly Howard

Laboratory Technician/Supervisor

Jason Som 12/11/2002 Development Engineer Jason Slone

Dates Conducted:

January 7, 2002

Objective:

Determine the amount of torque required to lever-out three different 36.0 mm modular head designs from the liner, as well as determining how much if any a Cobalt Reinforcement ring will strengthen design from a Titanium Reinforcement Ring.

Materials:

Part Name	Part Number	Lot Number	Size	Quantity
23 Constrained +5 Liner w/Cobalt Ring	investigational	815390	23 .	6
23 Constrained +5 Liner w/Ti-6Al-4V Ring		815390.	23	6.
CoCr Reinforcement Ring		R&D	23	6
Ti-6Al-4V Reinforcement Ring		R&D	23	6
36mm Full Sphere Modular Head		R&D	36	1 ·
36mm/35 flat Full Sphere Modular Head	Investigational	R&D	36/35	1
36mm/34.5 flat Full Sphere Modular Head	Investigational	R&D	36/34.5	1

The 23 Constrained Liners were manufactured complete at Biomet Warsaw. The Retaining Rings and Modular Head were manufactured at Biomet Warsaw in the Research and Development area. The rings were manufactured complete except for chemical etch, sterilization and packaging processes, which have no effect of this test.

Methods:

See Attached Sheet for Test Procedure

Calculations:

Lever-Arm:

The calculated lever-arm for this test was done using the CAD system. See Attached Figures with Sample Numbers. The constrained liner design was taken and rotated until the lever-out bar was horizontal. Then the head was constrained so that it must pop out of the liner perpendicular to the face of that liner. The maximum displacement was then used to determine where the Force from the actuator was being placed.

Percent Increase of CoCr Reinforcement Ring:

[(Average Torque Ti-6Al-4V)-(Average Torque CoCr)]/(Average Torque Ti-6Al-4V)

Results:

The results of the lever out test were as follows.

		Mechanical T	est 2439		
Specimen#	Maximum Displacement (in)	Maximum Recorded Force (lbs)	Calculated Lever Arm (in)	Calculated Torque (in- lbs)	Modular Head Size
4	0.652	41.6	3.216	133.8	
5	0.662	43.2	3.215	138.9	36/34.5
200			100 ZE 1		
	ESS 2017/10/EXS		10 SE SE DE SE	NAME OF THE OWNER.	•
6	0.687	43.5	3.213	139.8	
7	0.746	44.5	3.206	142.7	36/35.0
				37874	30/33.0
	7.055.0		77 di 28 di 28	360 B7 88 F	
8	0.720	40.5	3.209	130.0	36/36
	a de des		vale l	2000 1000	55/50

Note: Blocks in Gray are Liners with a Cobalt Chrome Reinforcement Ring;
Bold Numbers are maximum Torque

Conclusion:

As can be seen from the data the maximum amount of torque is acquired using a CoCr Reinforcement Ring with a 36/35.0 modular head. This scenario makes sense because it will displace a small amount of polyethylene when placed into the liner, but maintain the most amount of surface area when in a lever-out position. See tests reports MT2239 and MT2412 showing what the difference can be when using a full spherical head compared to a head that is not a complete sphere.

The 36/35.0 modular head shows the best results with either the CoCr or Ti-6Al-4V Reinforcement Rings. The CoCr Reinforcement Ring increases the leverout strength of this UHMWPE constrained liner design by roughly 9%.

Average Force vs. Displacement Displacement (in) :: 4.0 Force (lbs)

36 Full CoCr Ring ---- 36 Full TI Ring -38/35.0 CoCr Ring -36/34.5 CoCr Ring ----36/35.0 Ti Ring ---38/34.5 TI Ring -

1.2 ---- 36/34.5 (Sample ATI) ---- 36/34.5 (Sample 2TI) ----- 36/34.5 (Sample ACoCri) 0.8 Displacement (In) 0.2 (bdl) əਹਾoਜ

Force vs. Displacement

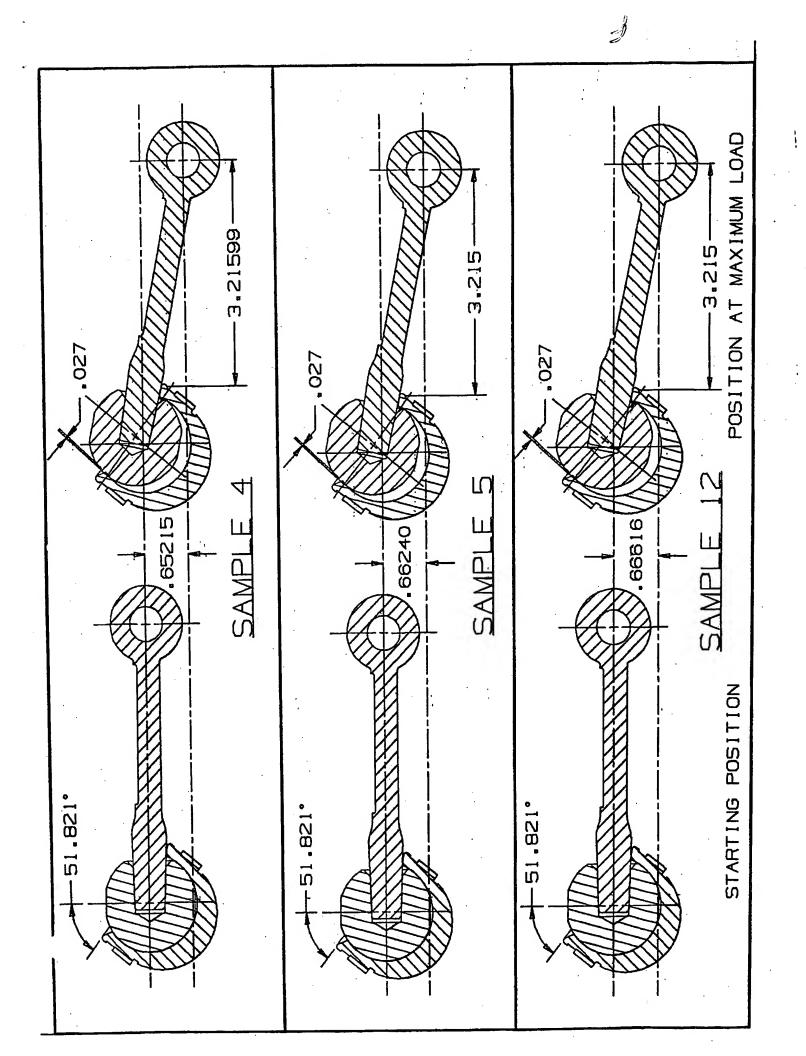
36/35.0 (Sample 2 TI) --- 36/35.0 (Sample / CoCr) --- 36/35.0 (Sample / CoCr) 7. 0.8 Displacement (in) 9.0 0.4 -36/35.0 (Sample / TI) 0.2 Force (lbs)

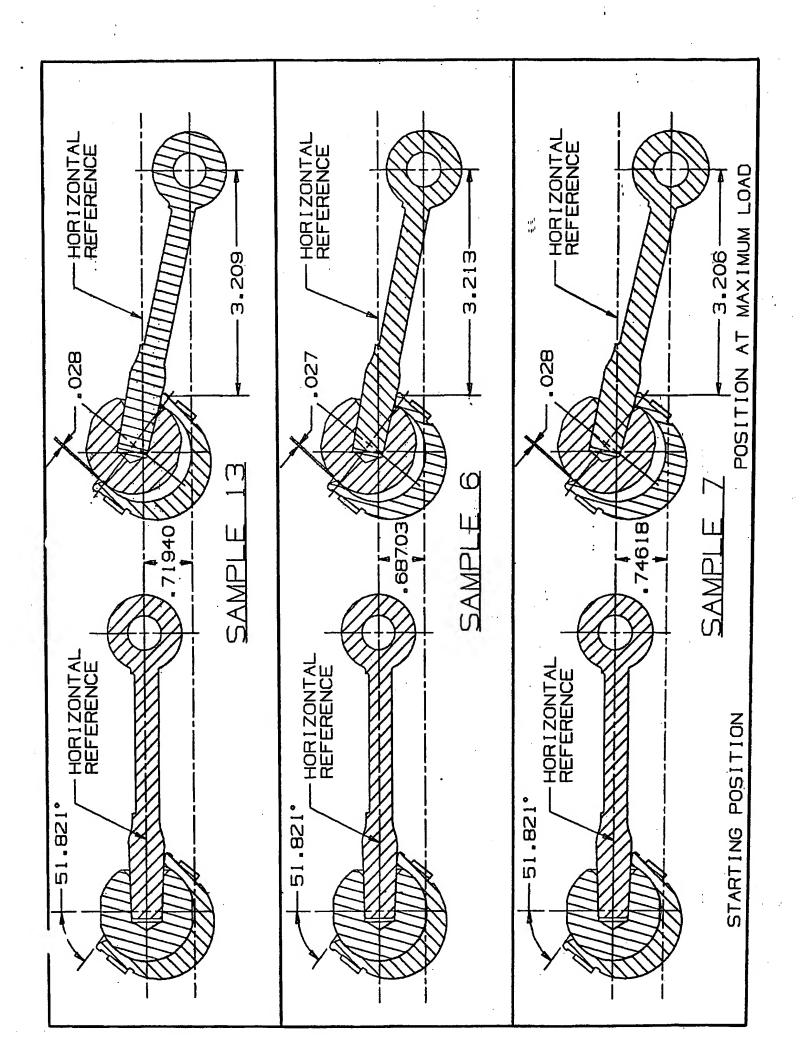
Force vs. Displacement

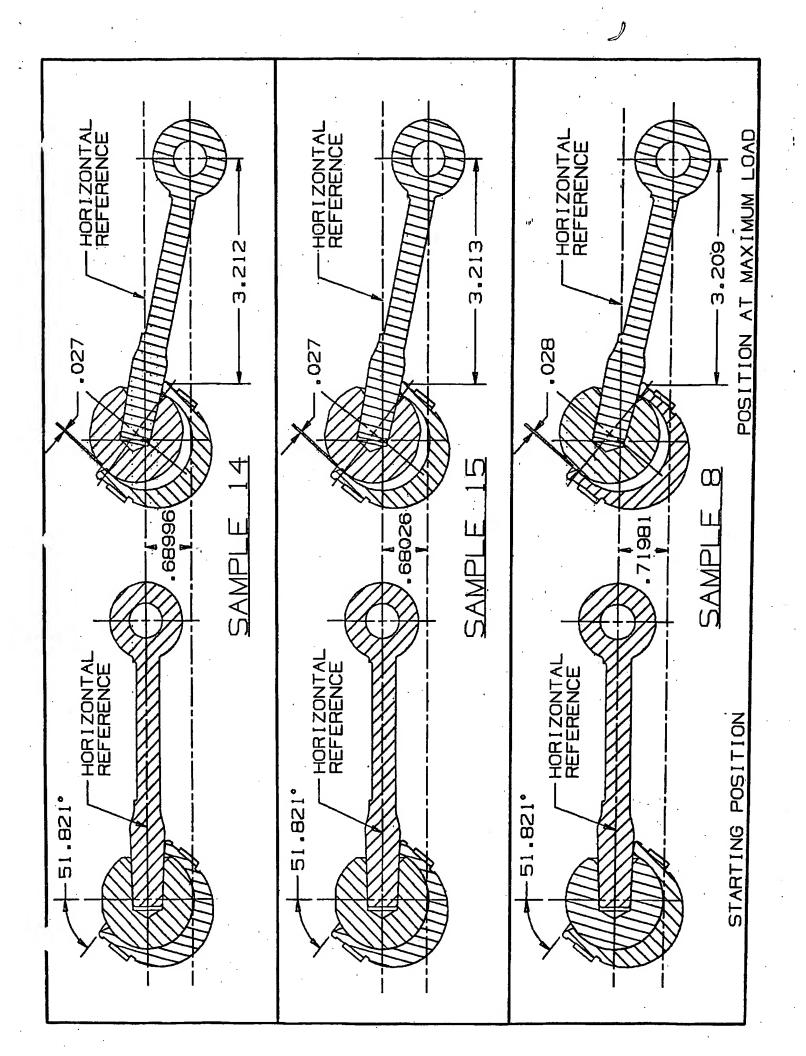
9.0 Displacement (in) 9.0 0.4 0.2 Force (lbs) - 0 40 35 30 25 Ġ 45

Force vs. Displacement

−36mm Full Head (Sample 1/TI) ——36mm Full Head (Sample 2/CoCr)







			36mn	36mm Constrained Liners	ed Liners			
Specimen 8	I taitial I D Dimension	I.D after Lla.N	Initial O.D Dimension	O.D after Llq.N	Initial O.D Ring Groove	O.D Ring Groove after Liq.N	2	Ring Material
Opporting in	-	. Er	0.83100	0.83123	1.5770	1.5775	1.6900	TI-6AI-4V
- (0.711.22	0.74533	0 82620	0.82687	1.5730	1,5725	1,6890	TI-6AL4V
7	0.717.0	0.7130	0,000	0 0 2 2 3 2	1 5700	1.5715	1.6890	T-64-4V
e0	0.71743	0.71366	0.02311	20020.0		0023	4 0000	TLEALAN
4	0.71764	0.71546	0.82649	0.826//	1.5/30	00,001	2000.	
×	0.71616	0.71731	0.82677	0.82779	1.5740	1,5750	1.6890	A+
	0 71789	0 71442	0.82350	0.82361	1.5710	1.5695	1.6895	T-6A-4V
- t	0.7.100	0.74787	0.82588	0.82701	1.5720	1.5730	1.6890	T-6A -4V
- ·	0.7.00	24400	0 82634	0.82698	1.5720	1.5725	1.6890	Ti-6AL4V
50	88717.0	0.7.030	0.0000	A 8762A	1 5720	1.5720	1.6870	ပုံ
6	0.71708	859L/10	0.62303	0.02027	0000	4 5736	4 8800	2
10	0.71763	0.71792	0.82627	0.82669	05/4.1	1.57.55	0600.1	3 6
	0.71791	0.71686	0.82613	0.82591	1.5730	1.5785	1.6870	i S
2:	0.7483	0 71701	0.82508	0.82619	1.5750	1.5730	1.6880	ပုံ ဝိ
4 5	0.7174	0.69682	0.82681	0.82805	1.5750	1.5760	1.6880	ပုံ ဝိ
2 ;	24460	0.74749	0.82617	0.82785	1.5730	1.5740	1.6870	ပုံဝိ
± ¥	0.71638	0.71824	0.82548	0.82641	1.5720	1.5725	1.6885	ပုံ
	0.71708	0.71752	0.82550	0.82605	1.5750	1.5760	1.6890	ပုံ ပိ
4	0.71765	0.71917	0.82868	0.82963	1,5750	1.5750		
60	0.71688	0,71789	0,82553	0.83822	1.5750	1.5755		
19	0.71807	0.71841	0.82865	0.82875	1.5730	1,5750		
20	0,71748	0.71839	0.82678	0.82733	1.5720	1.5730		

:

	NOT Put in Liquid Nitrogen																			
Difference	-0.0005	0.0005	-0.0015	0.0000	-0.0010	0.0015	-0.0010	-0.0005	00000	-0.0005	-0.0035	0.0020	-0.0010	-0.0010	-0.0005	-0.0010	0.0000	-0.0005	-0.0020	- D 0040
60	12	9	2		•	_	_	7.	*	<u> </u>			- 7	_	_	<u></u>			=	99
Difference	9,000	-0.00	0.000	0000	-0.0010	00.0	-0.00	000'0-	-0.00	-0.00	0.000	-0.00	-0.00	-0.00	-0.00	0000	-0.001	-0.012	0000	000.0-
Difference	-0.0019	0.0024	0.0018	0.0022	-0.0011	0.0035	-0.0016	0.0020	0.0007	-0.0003	0.0011	-0.0007	0.0203	-0.0013	-0.0019	-0.0004	-0.0015	-0.0010	-0.0003	60000-
Specimen #	-	~	ო	4	10	ø	_	€	۵	2	Ŧ	12	£	7	15	16	4	13	18	70

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